

Current and contemporary seismic design methods: a comparative review

Gerard J. O'Reilly, Davit Shahnazaryan
IUSS Pavia, Italy



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Scuola Universitaria Superiore Pavia

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CENTRE FOR TRAINING AND
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OF SEISMIC RISK

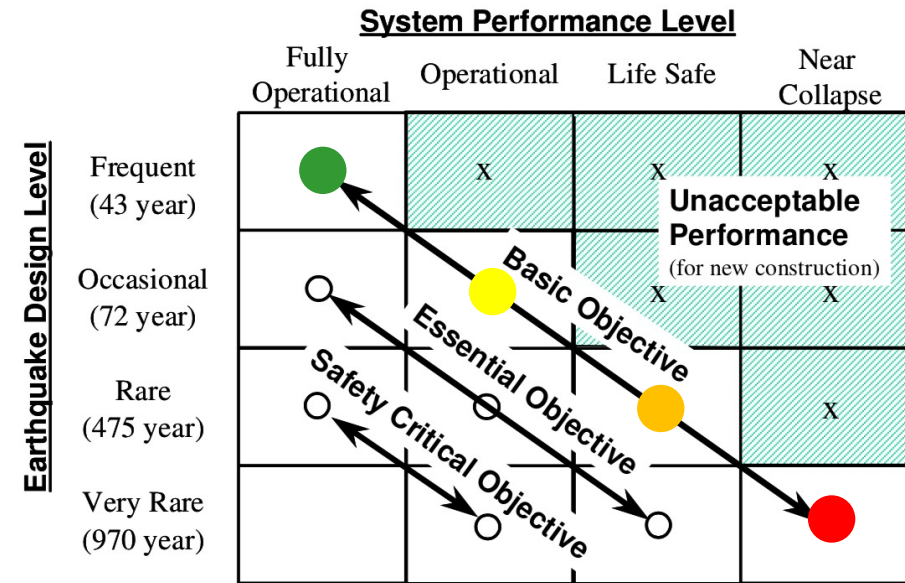
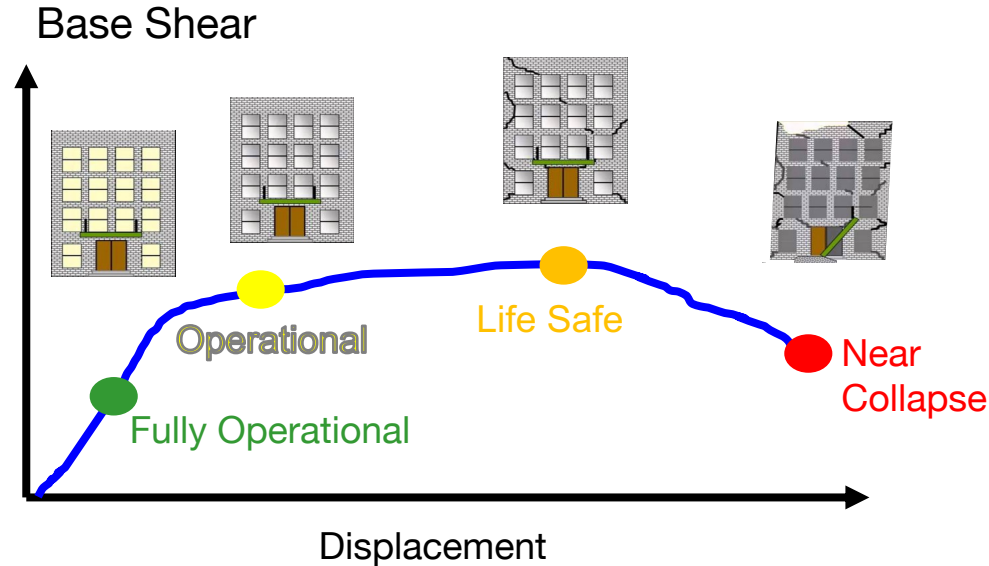
Introduction

- In earthquake engineering, we need to be able to communicate with the decision-makers, building owners and stakeholders
- We strive towards acceptable levels of safety and loss
- This must be quantifiable through risk communication and also insurance terminology
- We need appropriate tools to tackle the issue



Introduction

- Seismic performance has traditionally looked at the idea of defining limit states and linking them to returns periods of shaking
- This is the basis of many modern building codes around the world

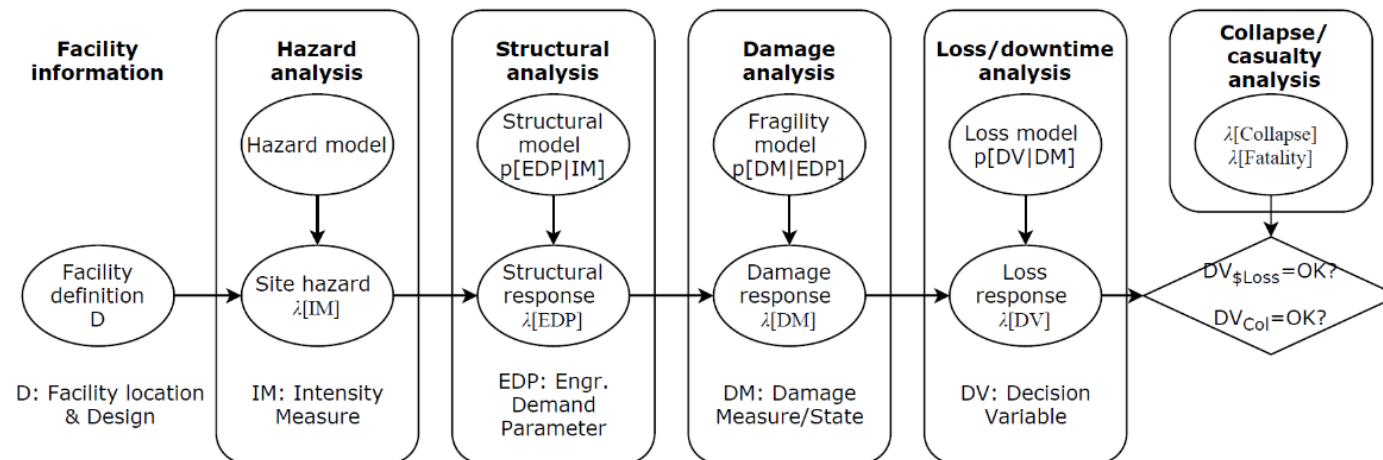


From SEAOC Vision 2000 document

Introduction

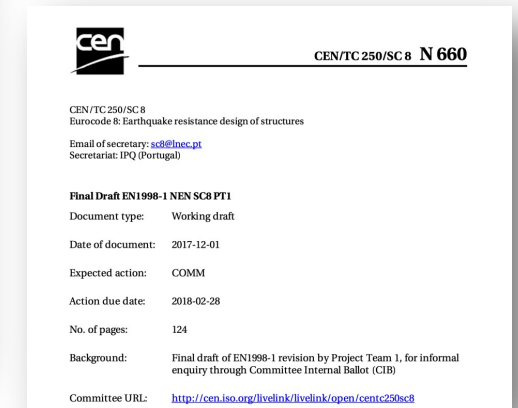
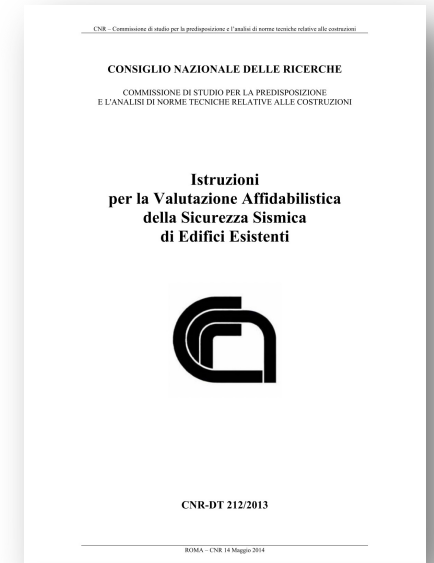
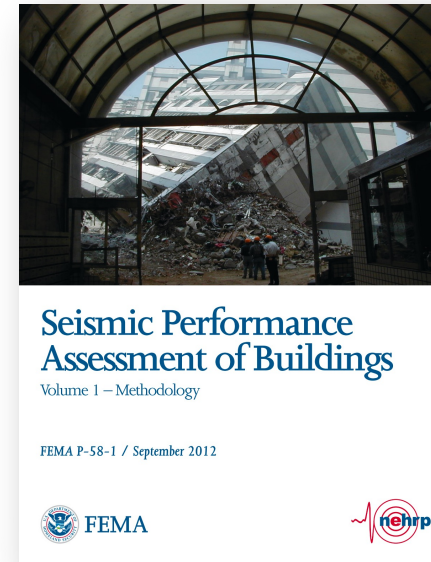
- In recent years, a more probabilistic approach is being favoured and quantifies the performance in a *risk* sense
- Its definition of “failure” is flexible, allowing consistent consideration across all pertinent limit states
- It also utilises performance metrics that are useful in other fields:
 - Average annual risk of collapse (or fatality)
 - Average annual loss (direct or indirect?)
 - Downtime

$$\lambda_f = \int_0^{+\infty} P[f|IM = s] |dH(s)|$$



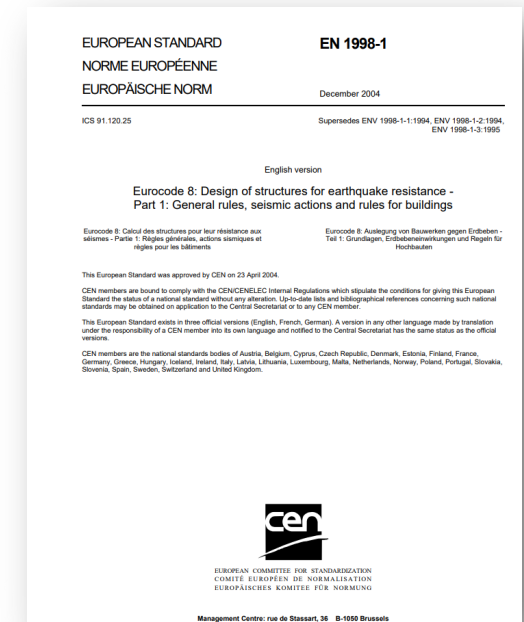
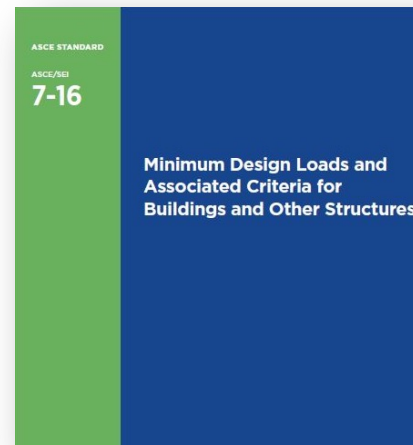
Introduction

- Popular within academic research or specialised reports rather than widespread code implementation for practitioners to use
- Mainly due to the probabilistic nature of the framework and its computationally expensive implementation in certain situations
- Some examples:
 - CNR-DT 212/2013
 - FEMA P-58 - 2012
 - New Eurocode 8 (Annex F)
- If we use these methods and performance metrics, what are the limits or targets ?



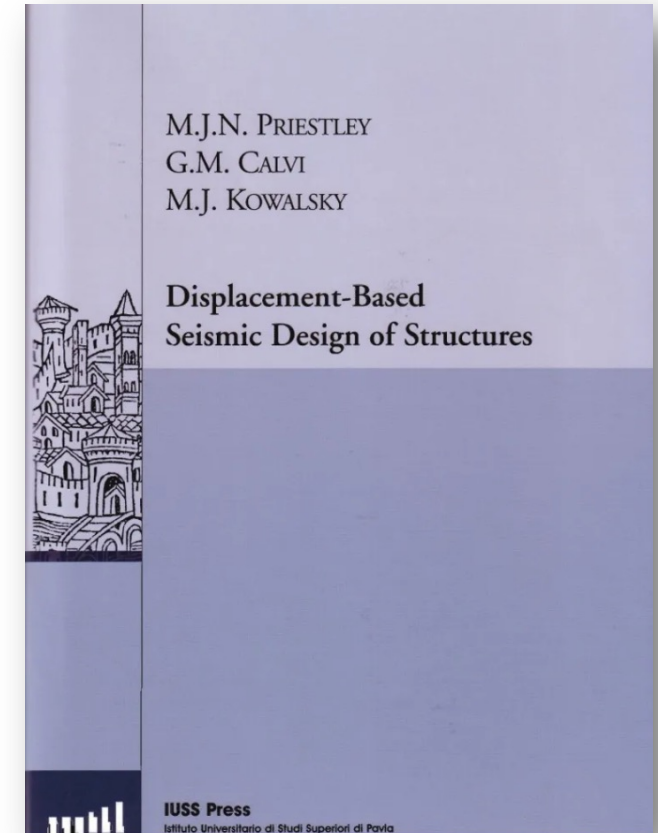
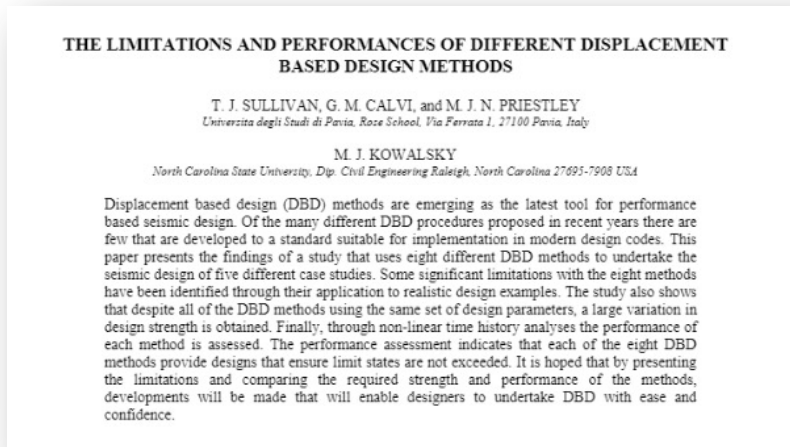
Current design approaches

- Force-based design (FBD) methods
 - Eurocode 8
 - 475 and 95 years for no-collapse and damage limitation
 - New Zealand's NZS1170
 - 500 and 25 years for ultimate and serviceability limit states
 - ASCE 7-16
 - Using a risk-targeted spectrum (see later)



Current design approaches

- FBD – not reasonable to quantify expected ductility and spectral demand reduction via unique behaviour factors
- Priestley et al. (2007) proposed using ductility- and typology-dependent spectral reduction approach
- This was the so-called displacement-based design (DBD) approach
- FBD and DBD solutions may be refined to be more in line with risk-targeted objectives



Critical Review

- Some of the more notable methods available are examined:
 - FBD – force-based design implemented in Eurocode 8 (and others)
 - DDBD – displacement-based design advocated by Priestley et al. (2007)
 - RTBF – risk-targeted behaviour factors by Kennedy and Short (1994) and Cornell (1996)
 - CPBD – conceptual performance-based design by Krawinkler et al. (2006)
 - RTS – risk-targeted spectra by Luco et al. (2007)
 - YFS – yield frequency spectra by Vamvatsikos and Aschheim (2016)
 - RTSA – risk-targeted seismic action by Žižmond and Dolšek (2019)
 - IPBSD – integrated performance-based seismic design by Shahnazaryan and O'Reilly (2021)

Performance objectives (PO)

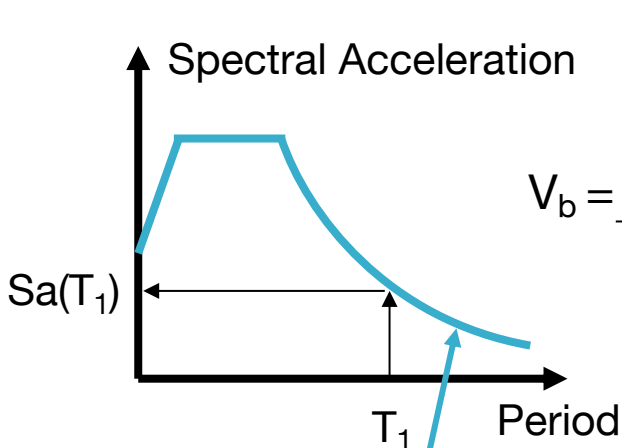
- Primary quantity that each design method targets, limits or bases itself upon
 - Classic methods focus on a specific structural response at a given return period
 - More recent methods are integrating risk aspects like annual probability or economic loss

	IPBSD	FBD	DDBD	RTBF	CPBD	RTS	YFS	RTSA-D	RTSA-I
PO	λ_c λ_v	$E[D T_R]$ $E[R T_R]$	$E[D T_R]$	CMR λ_c	$E[L T_R]$ $P[C T_R]$	λ_c	λ_0 λ_u	λ_c	λ_c
H	$H(Sa(T))$	UHS	UHS	UHS $H(AvgSa)$	$H(Sa(T_1))$	UHS	$H(Sa(T_1))$	$H(Sa(T_1))$	$H(Sa(T_1))$ & UHS
NL	Assume μ and q_s and get q_u from SPO2IDA	Traditional q factors	Equivalent viscous damping	Calibrated q factors	NLRHA	Traditional q factors	SPO2IDA	Assume r_s and μ_{NC} and calculate C_1 from IDA	Assume r_s and μ_{NC} and calculate C_1 from IDA (Equivalent q factor)
DD	Moderate	Easy	Easy	Easy	Very Extensive	Easy	Moderate	Extensive	Extensive
FLX	Flexible	Limited	Flexible	Limited	Flexible	Limited	Flexible	Flexible	Flexible
PBEE	Yes	No	No	Yes	Yes	No	Yes	Yes	Yes



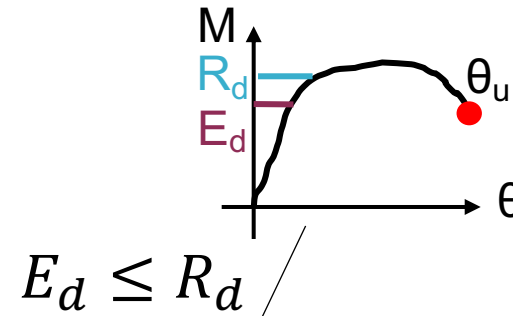
Performance objectives (PO)

- Starting first with the classic methods, what are the performance objectives?
- These are typically the expected response at known return periods (T_R): $E[R | T_R]$
 $E[D | T_R]$

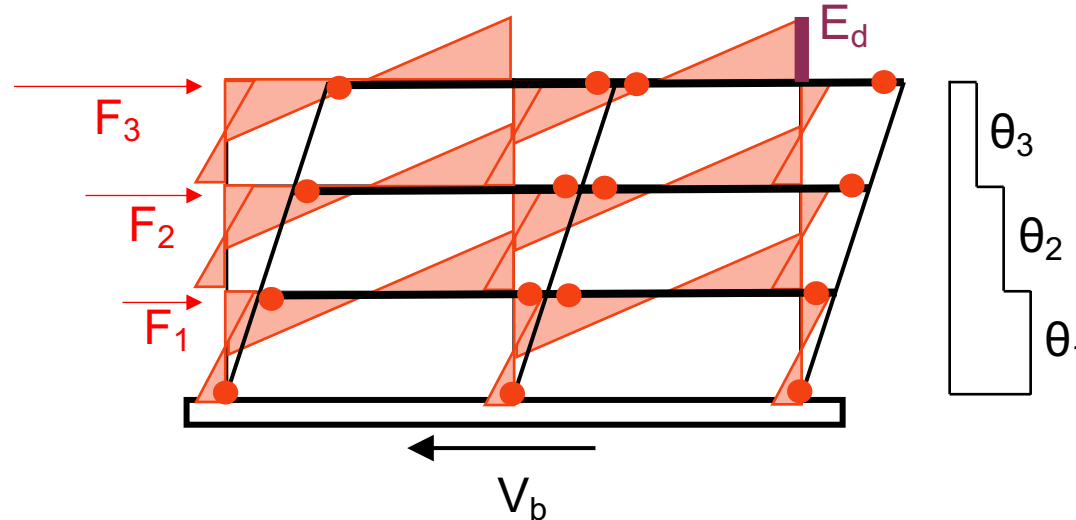


$$V_b = \frac{Sa(T_1)W}{q}$$

Response is checked for this return period



Make sure our sections have enough “kN”s or “kNm”s resistance



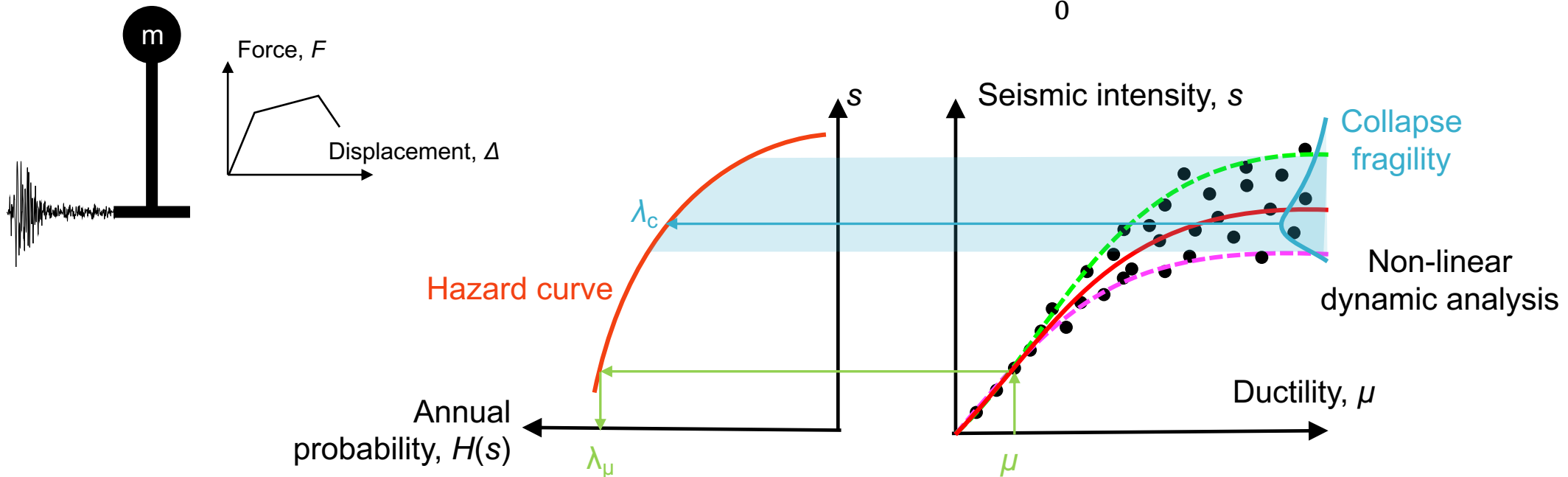
Depending on the type of non-structural element (NSE) and its connectivity, we have:

- Brittle NSEs: $\theta_{max} \leq 0.50\%$
- Ductile NSEs: $\theta_{max} \leq 0.75\%$
- Special or no NSEs: $\theta_{max} \leq 1.00\%$

Performance objectives (PO)

- More novel methods consider the performance across many intensity levels
- They integrate with the hazard curve to get the annual probability
- Methods based on this are risk-targeted

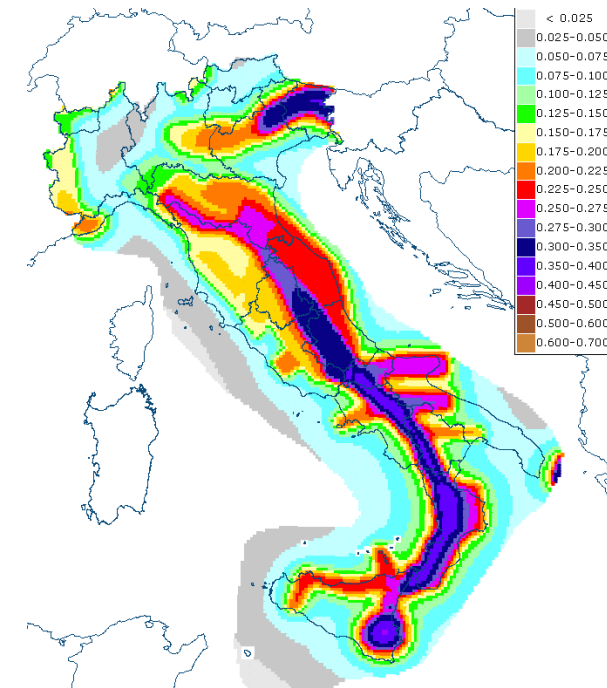
$$\lambda_f = \int_0^{+\infty} P[f|IM = s] |dH(s)|$$



Hazard (H)

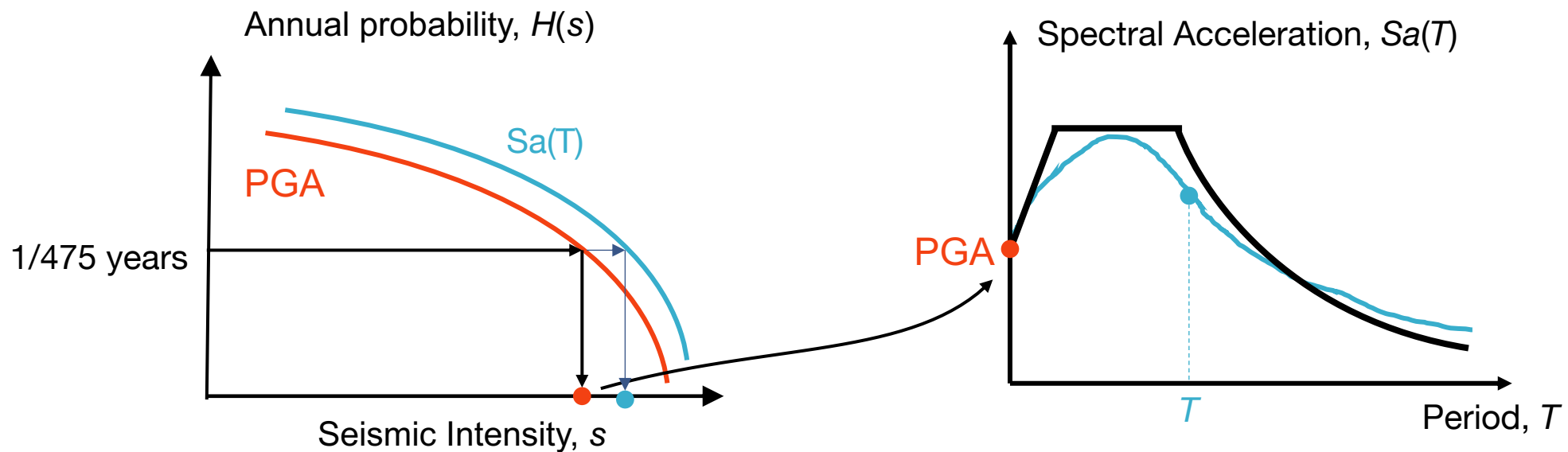
- How seismicity is characterized during design
 - Several of the methods employ uniform hazard spectrum (UHS)
 - Others use a hazard curve associated with an intensity measure, $H(\bullet)$

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PO	λ_c λ_v	$E[D T_R]$ $E[R T_R]$	$E[D T_R]$	CMR λ_c	$E[L T_R]$ $P[C T_R]$	λ_c	λ_θ λ_μ	λ_c	λ_c
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Hazard (H)

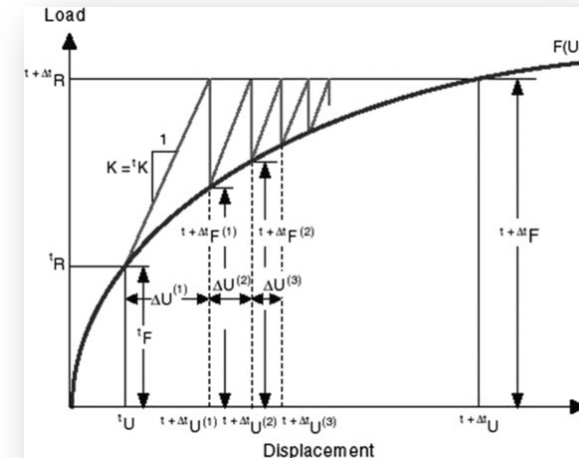
- The main difference here is whether we should consider the performance across all intensities via the hazard curve
- Or simply choose a few and check for those
- Are simplified code expressions for UHS actually representative of hazard analysis?



Accounting for non-linearity (NL)

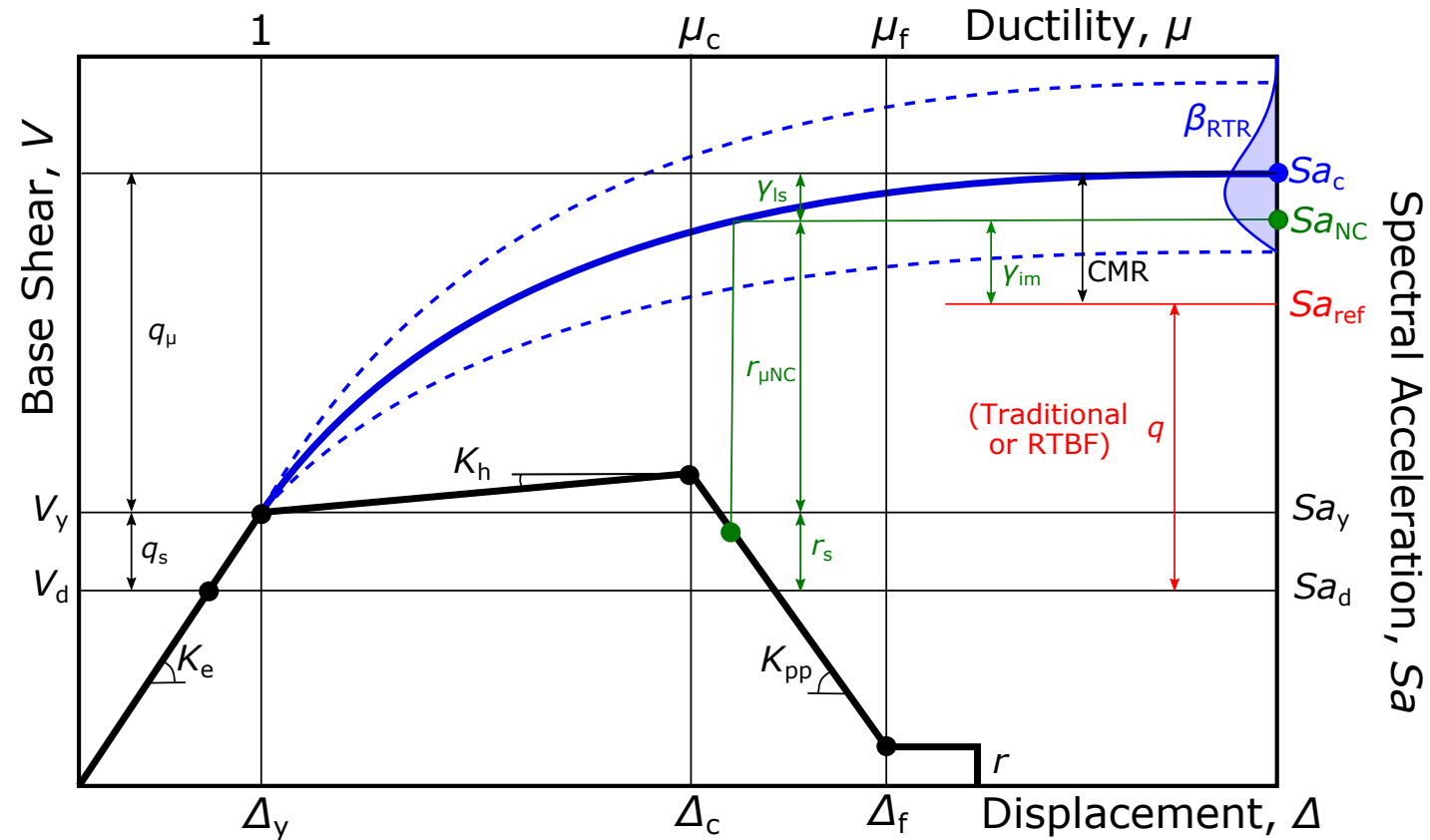
- How ductile structure behaviour is accounted for:
 - Reduce design forces via q -factors?
 - Use some proxy models?

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Accounting for non-linearity (NL)

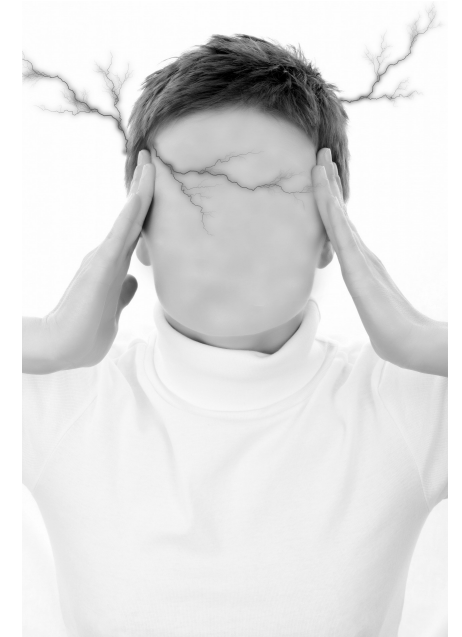
- One of the biggest challenges in simplified seismic design is how to relate the non-linear response of the system to its elastic SDOF equivalent



Relative difficulty and directness (DD)

- How difficult the method is – e.g., NLRHA required?
- How direct the method is – e.g., Multiple iterations required?

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FLX	Flexible	Limited	Flexible	Limited	Flexible	Limited	Flexible	Flexible	Flexible
PBEE	Yes	No	No	Yes	Yes	No	Yes	Yes	Yes



Flexibility and PBEE compliant?

- Flexibility - FLX
 - Ease of tailoring design targets beyond what it has been developed for so far
- PBEE
 - Is the method risk-consistent?

	IPBSD	FBD	DDBD	RTBF	CPBD	RTS	YFS	RTSA-D	RTSA-I
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In conclusion...

- This paper presented a review of classic design approaches and methods available in the literature
- Current design methods deal with design without adequately accounting for the probabilistic nature of the problem
- More contemporary risk-based seismic design approaches are available

